

**Fermilab**

PPD/MD/Engineering Analysis Group

**A Preliminary Stress Calculation for the Cell Structure  
Used in Liquid Scintillator (Off-Axis)**

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**The Vertical Cell**

For the vertical cell, we could assume that the liquid weight will be holding by themselves. Then, the only load seen by the sidewall will be the hydrostatic load. The Table 1 shows the maximum stress for a given wall thickness based on 17.5 m x 17.5 m plane, proposed in reference (1).

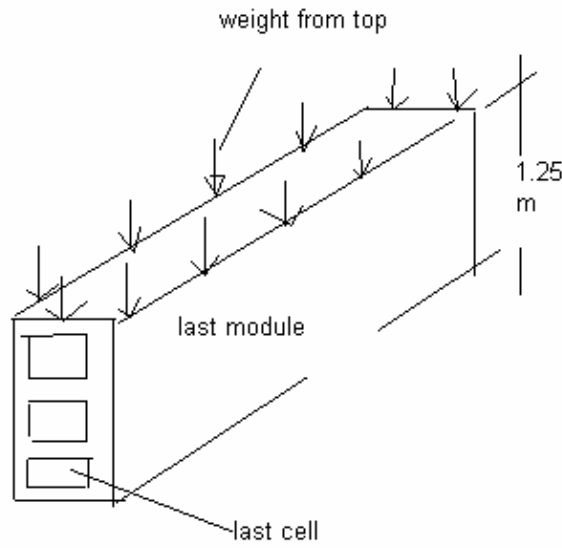
Table 1 The Vertical Orientation for 17.5m x 17.5m Plane  
With 4.5 cm Cell Size

Wall Thickness (mm)	Maximum Stress (psi)
1	21,169
2	5,292
3	2,352
4	1,323

**The Horizontal Cell**

For the horizontal cell, there will be two possible scenarios. The first one is to assume the liquid holding itself within its own module only. The load transfer between modules is primarily through the sidewall. Therefore, the total load at the lowest cell will be the hydrostatic load at 1.25 (m) plus the weight from top modules as following:

$$\sigma_t = \sigma_h(1.35m) + \sigma_w(weight)$$



where

$$\sigma_h = \frac{M}{S} = \frac{p \cdot l^2}{12} \bigg/ \frac{b \cdot t^3}{6} = \frac{1.49 \times 1.772^2}{12} \bigg/ \frac{1 \cdot 0.0787^3}{6} = 378 \text{ psi}$$

$$\sigma_w = \frac{W}{A} = \frac{(166 + 973) \cdot 14 \cdot 9.8}{2 \cdot 17.5 \cdot 0.002} = 2.23 \times 10^6 (\text{pascal}) = 323 \text{ psi} , \text{ then}$$

The total stress for horizontal orientation with  $t=2$  mm will be

$$\sigma_t = \sigma_h + \sigma_w = 378 + 323 = 701 \text{ psi}$$

The second scenario, which is most unlikely case, is to assume the liquid holding themselves just like the vertical one. The reasoning is that the cell divider could be very flexible. The load transfer is primarily relied on the liquid itself not sidewall. Then, the maximum stress for sidewall will be the same as the vertical orientation as listed in Table 1.

## Conclusion

The conclusion from this preliminary study shows that the vertical cell will be the driving force for the design of the wall thickness. In general, the tensile strength for PVC material is ranged from 5,000 psi to 12,000 psi, depended upon of the its material and the fabrication. As an example, if we use a PVC with 20% glass fiber reinforced, the tensile strength is about 10,000 psi. By assuming a safety factor of 2, the allowable will be 5,000 psi. The 2 mm wall thickness will be adequate.

## Reference

“An Alternative Version of a Liquid Scintillator Detector: Totally Active Configuration”. Stan Wojcicki, Stanford University, Off-Axis-Note-scint-28, Feb. 21,2004

## Appendix A : The detail calculation for the vertical orientation

**Case 1: Assuming all modules are continuously stacking up (gluing) together to form a 17.5 m x 17.5 m plane**

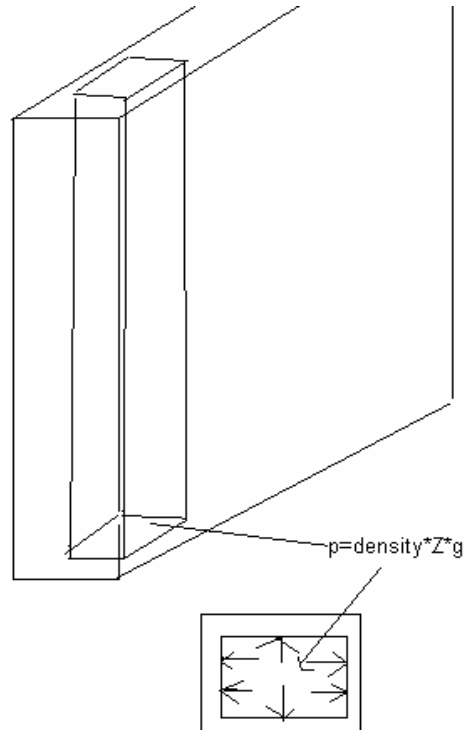
Given: mineral oil SG=0.84

<b>density</b>	<b>p hydrostatic pressure at 17.5 m</b>	$p = \text{density} \cdot g \cdot Z(17.5 \text{ m})$
840 kg/m <sup>3</sup>	144060 pascal or	
	20.90856 psi	

**For a simple model, a square box with 4.5 cm length subjected to 20.9 psi pressure with 2 mm wall thickness**

<b>q</b>	<b>a</b>	<b>b</b>
144060 pascal	4.500 cm	4.500 cm
20.90856 psi	1.772 inch	1.772 inch

t (wall thickness)	moment	S	maximum bending stress	Maximum deflection	
<b>1.000</b> mm					
0.039 inch	5.47	0.000258	<b>21169.92</b> psi	<b>0.105485</b> inch	2.68 mm
<b>2.000</b> mm					
0.079 inch	5.47	0.001033	<b>5292.48</b> psi	<b>0.013186</b> inch	0.33 mm
<b>3.000</b> mm					
0.118 inch	5.47	0.002325	<b>2352.213</b> psi	<b>0.003907</b> inch	0.10 mm
<b>4.000</b> mm					
0.157 inch	5.47	0.004133	<b>1323.12</b> psi	<b>0.001648</b> inch	0.04 mm



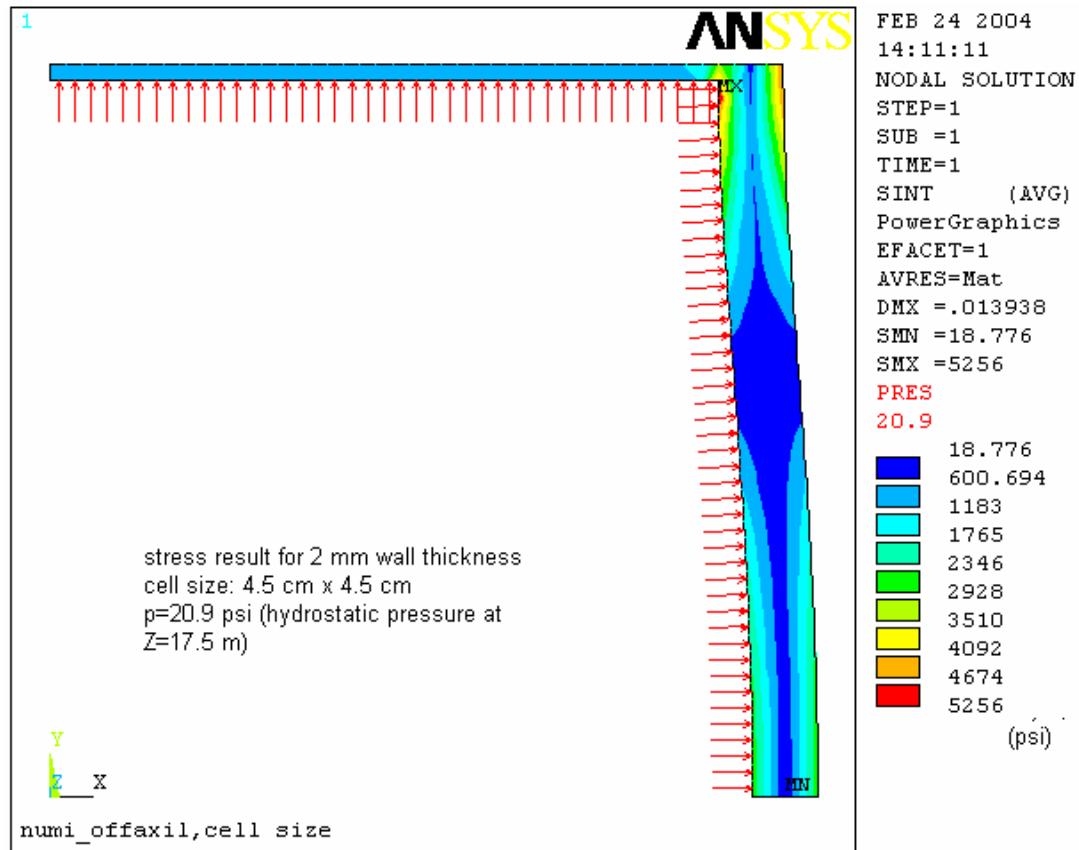


Figure 1 The stress result from ANSYS for a t=2 mm